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# **TEST REPORT**

**Test Method:** 

CAN/ULC-S102.2:2018-REV1, Standard Method of Test for Surface Burning Characteristics of Flooring, Floor Coverings and Miscellaneous Materials and Assemblies

**Rendered To:** 

**Product Description:** 

**Report Number:** 

**Original Issue Date:** 

Test Date:

Pages:



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## I. SCOPE

This test report contains the results from a specimen tested in accordance with CAN/ULC-S102.2, Standard Method of Test for Surface Burning Characteristics of Flooring, Floor Coverings, and Miscellaneous Materials and Assemblies. The results of CAN/ULC-S102.2 testing are commonly used by building code officials and regulatory agencies to determine whether interior finish materials are suitable for their intended application.

#### **II. TEST SPECIMENS**

Test specimens should be representative of the material which the test is intended to examine. All test specimens should be approximately 10mm narrower than the interior width of the tunnel and 7315  $\pm$  15 mm in length. The maximum allowable thickness is 65mm. The test specimen can be provided in a continuous, unbroken length or multiple sections that will be butted together. Prior to testing, the specimens are conditioned to a constant mass in an environment that is held at 23  $\pm$  3 °C (73.4  $\pm$  5.4 °F) and 50  $\pm$  5% relative humidity.

TEST SPECIMEN INFORMATION			
Description			
Samples Selected By			
Date Received			
Conditioning Time			
Specimen Size (in.)			
Continuous / Sectioned			
Number of Sections			
Avg. Total Weight (lbs.)			
Average Thickness (in.)			
Color			
Exposed Surface			
Mounting Method			
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\* Information provided by the Client



## **III. PROCEDURE**

The tunnel is preheated to  $85 \pm 5$  °C ( $185 \pm 9$  °F) as measure by a thermocouple embedded in the backwall of the furnace at 7090 mm (23.3 ft) from the centerline of the burner. The tunnel is then cooled to  $40 \pm 3$  °C ( $104 \pm 5.4$  °F) as measured by a thermocouple embedded in the backwall of the furnace at 4000 mm (13.1 ft) downstream of the centerline of the burner.

After the tunnel has cooled to required temperature range, the tunnel lid is lifted, and the test specimen is placed on the floor of the tunnel. The specimen is with the side that will be exposed to the flame facing upward.

Once the sample has been loaded into the test chamber, the lid is lowered, and a  $1.2 \pm 0.025$  m/s (236.2 ± 4.9 ft/min) airflow is established. The test specimen is preheated for approximately 2 minutes prior to applying the 90 kW burner. The burner is positioned at the front end of the tunnel. It has two ports that point downward at a 45° angle toward the face of the specimen. An air ramp is placed at the front end of the specimen to reduce air eddies and to prevent low density material from being blown away from the burner.

After the 2-minute preheat, the burner is ignited, and it remains on for the duration of the 10-minute test. The flame is tracked by an observer, referred to as the Reader, as it progresses down the length of the tunnel. Smoke density is measured with the use of the photometer system on the exhaust duct. Temperature data is recorded throughout the test by a thermocouple probe that is 7000 mm (23 ft) from the centerline of the burner and approximately 25mm (1 in.) below the upper ledges of the tunnel.

#### **IV. TEST RESULTS**

In CAN/ULC-S102 testing, test results for individual burns are reported as Flame Spread Value (FSV) and Smoke Developed Value (SDV). The average indices, that are derived from a minimum of three individual burns, are reported as Flame Spread Rating (FSR) and Smoke Developed Classification (SDC).

The Flame Spread Value is derived by plotting the flame spread distance versus time. Only progressive flame spread is plotted. The total area  $(A_T)$  under the flame spread distance-time plot is determined by ignoring any flame front recession. The calculation of FSV is described below:

When  $A_T \le 29.7 \text{ m} \cdot \text{min}$ :FSV =  $1.85 * A_T$ When  $A_T > 29.7 \text{ m} \cdot \text{min}$ :FSV =  $1640/(59.4 - A_T)$ 



The Smoke Developed Value is derived by plotting the photoelectric cell readings versus time. The area under the curve for the tested material is then divided by the area under the curve for select-grade red oak flooring. The resulting value is then multiplied by 100.

The Flame Spread Rating is determined by averaging a minimum of three individual Flame Spread Values and rounding that average to the nearest multiple of 5. The Smoke Developed Classification is determined by averaging a minimum of three individual Smoke Developed Values and rounding that average to the nearest multiple of 5.

FLAME SPREAD RATING (FSR)	SMOKE DEVELOPED CLASSIFICATION (SDC)		

Test Start Date	
Test End Date	
Equipment Operator	
Flame Spread Reader	

	Burn #1	Burn #2	Burn #3
Ignition Time (s)			
Flame Spread Value (FSV)			
Smoke Developed Value (SDV)			
Maximum Temperature (°C)			
Maximum Temperature (°F)			
Time to Maximum Temperature (min)			
Maximum Flame Spread Distance (m)			
Maximum Flame Spread Distance (ft)			
Time to Maximum FS Distance (min)			



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## **V. OBSERVATIONS**

**During Test** 

After Test

Note: Reported observation distances are relative to the entire length of the test specimen.

#### **VI. REMARKS**



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## **VII. GRAPHS AND INDIVIDUAL BURN DATA**

Test Room Temperature (°F):

Test Room Humidity (%RH):

Note: Distances on this page are reported in meters.

Test Report No.:

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Test Room Temperature (°F):

Test Room Humidity (%RH):

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#### **VIII. DISCUSSION**

#### CAN/ULC-S102.2 Standard Language and Disclaimers

The following language was taken directly from the CAN/ULC-S102.2 standard. It has been included for information purposes.

Smoke Developed Value (SDV) and Flame Spread Value (FSV) are recorded in this test. However, there is not necessarily a relationship between these two measurements. – CAN/ULC-S102.2:2018-REV1, Section 1.4

This method defines the relative surface burning characteristics under specified test conditions. Although the procedure is applicable to materials, products and assemblies used in building construction for development of comparative surface spread of flame data, test results may not reflect the relative surface burning characteristics of tested materials under all building fire conditions. – CAN/ULC-S102.2:2018-REV1, Section 3.1

The "fire hazard" of any material in the light of present knowledge cannot be evaluated on the basis of any one test. A body of tests, each measuring one or more characteristics of a material, product, or assembly, may be needed for full assessment. These assessments are intended as aids to those who have the responsibility for determining acceptable levels of potential hazard. The overall fire hazard of a material as it is to be used can only be determined by an analysis of its behavior under several test conditions in addition to further analysis which includes consideration of building construction, occupancy, location and fire protection features. – CAN/ULC-S102.2:2018-REV1, Section 3.2

#### **IX. AUTHORIZED SIGNATURES**

Christopher Kaiser Laboratory Technician II - Fire

**Reviewed and Approved By:** 

Chris Palumbo Sr. Manager of Product Testing Date

Date



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## X. REVISION HISTORY

Revision Number	Date	Summary
0		Original Report Issued



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**XI. APPENDIX** 

Test Room Temperature (°F):

Test Room Humidity (%RH):

In accordance with Section A1.1.4, screening tests were conducted to determine whether mounting the product on the floor or mounting the product on the ceiling produced a higher flame spread value. The data above is from the screening test that was conducted on the ceiling of the test chamber. It has been included for informational purposes.